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NATIONAL DAM SAFETY PROGRAM, HOPE LAKE DAM (NJ 00796) DELAWARE --ETC(U)
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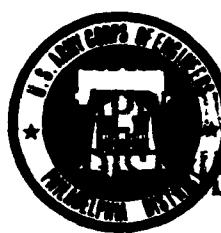
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DELAWARE RIVER BASIN
BEAVER BROOK, WARREN COUNTY
NEW JERSEY

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HOPE LAKE DAM NJ 00796

PHASE 1 INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM



FILE COPY

DEPARTMENT OF THE ARMY

Philadelphia District
Corps of Engineers
Philadelphia, Pennsylvania

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report cites results of a technical investigation as to the dam's adequacy. The inspection and evaluation of the dam is as prescribed by the National Dam Inspection Act, Public Law 92-367. The technical investigation includes visual inspection, review of available design and construction records, and preliminary structural and hydraulic and hydrologic calculations, as applicable. An assessment of the dam's general condition is included in the report. → pg. 1		



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21 AUG 1981

Honorable Brendan T. Byrne
Governor of New Jersey
Trenton, New Jersey 08621

Dear Governor Byrne:

Inclosed is the Phase I Inspection Report for Hope Lake Dam in Warren County, New Jersey which has been prepared under authorization of the Dam Inspection Act, Public Law 92-367. A brief assessment of the dam's condition is given in the front of the report.

Based on visual inspection, available records, calculations and past operational performance, Hope Lake Dam, initially listed as a high hazard potential structure, but reduced to a significant hazard potential structure as a result of this inspection, is judged to be in very poor overall condition. The dam's spillways are considered inadequate because a flow equivalent to 5 percent of the Spillway Design Flood (SDF) would cause the dam to be overtopped. To ensure adequacy of the structure, the following actions, as a minimum, are recommended:

a. The spillway's adequacy should be determined by a qualified professional consultant engaged by the owner using more sophisticated methods, procedures and studies within six months from the date of approval of this report. Within three months of the consultant's findings remedial measures to ensure spillway adequacy should be initiated. In the interim, during periods of unusually heavy precipitation, around the clock surveillance should be provided.

b. Within three months from the date of approval of this report the owner should engage a qualified professional consultant to perform the following:

(1) Investigate the cause of the seepage and wet, soft areas at the downstream toe of the dam.

(2) Design procedures for and inspect the removal of the trees and their roots from the entire embankment.

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Honorable Brendan T. Byrne

(3) Design procedures for and inspect the construction of erosion protection on the upstream slope of the dam.

(4) Design procedures for the repair or replacement of the gated and ungated spillways where considerable erosion and seepage are taking place.

(5) Design channels to reroute the flowing water away from the toe of the dam.

(6) Establish procedures and supervise backfilling of the embankment sections on either side of the stoplog spillway.

c. Within one year from the date of approval of this report the owner should engage a qualified professional consultant to design and supervise installation of adequate means to drain the reservoir in case of emergency.

d. Within thirty days from the date of approval of this report the following remedial actions should be initiated:

(1) Clear debris and trees from the spillway discharge channels and maintain the channels free from debris.

(2) Clear brush and uncontrolled vegetation from slopes of the dam and keep the slopes free from all debris.

(3) Clear trees and brush for some distance downstream from the toe of the dam and from the banks of the discharge channels for some distance downstream from the spillways.

e. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam, within one year from the date of approval of this report.

f. An emergency action plan and warning system should be developed which outlines actions to be taken by the owner to minimize the downstream effects of an emergency at the dam within six months from the date of approval of this report.

A copy of the report is being furnished to Mr. Dirk C. Hofman, New Jersey Department of Environmental Protection, the designated State Office contact for this program. Within five days of the date of this letter, a copy will also be sent to Congressman Courter of the Thirteenth District. Under the provision of the Freedom of Information Act, the inspection report will be subject to release by this office, upon request, five days after the date of this letter.

Additional copies of this report may be obtained from the National Technical Information Services (NTIS), Springfield, Virginia 22161 at a reasonable cost. Please allow four to six weeks from the date of this letter for NTIS to have copies of the report available.

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Honorable Brendan T. Byrne

An important aspect of the Dam Inspection Program will be the implementation of the recommendations made as a result of the inspection. We accordingly request that we be advised of proposed actions taken by the State to implement our recommendations.

Sincerely,



1 Incl
As stated

ROGER L. BALDWIN
Lieutenant Colonel, Corps of Engineers
Commander and District Engineer

Copies furnished:

Mr. Dirk C. Hofman, P.E., Deputy Director
Division of Water Resources
N.J. Dept. of Environmental Protection
P.O. Box CN029
Trenton, NJ 08625

Mr. John O'Dowd, Acting Chief
Bureau of Flood Plain Regulation
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HOPE LAKE DAM (NJ00796)

CORPS OF ENGINEERS ASSESSMENT OF GENERAL CONDITIONS

This dam was inspected on 21 April 1981 by Anderson-Nichols and Co. Inc., under contract to the State of New Jersey. The State, under agreement with the U.S. Army Engineer District, Philadelphia, had this inspection performed in accordance with the National Dam Inspection Act, Public Law 92-367.

Hope Lake Dam, initially listed as a high hazard potential structure, but reduced to a significant hazard potential structure as a result of this inspection, is judged to be in very poor overall condition. The dam's spillways are considered inadequate because a flow equivalent to 5 percent of the Spillway Design Flood (SDF) would cause the dam to be overtopped. To ensure adequacy of the structure, the following actions, as a minimum, are recommended:

a. The spillway's adequacy should be determined by a qualified professional consultant engaged by the owner using more sophisticated methods, procedures and studies within six months from the date of approval of this report. Within three months of the consultant's findings remedial measures to ensure spillway adequacy should be initiated. In the interim, during periods of unusually heavy precipitation, around the clock surveillance should be provided.

b. Within three months from the date of approval of this report the owner should engage a qualified professional consultant to perform the following:

(1) Investigate the cause of the seepage and wet, soft areas at the downstream toe of the dam.

(2) Design procedures for and inspect the removal of the trees and their roots from the entire embankment.

(3) Design procedures for and inspect the construction of erosion protection on the upstream slope of the dam.

(4) Design procedures for the repair or replacement of the gated and ungated spillways where considerable erosion and seepage are taking place.

(5) Design channels to reroute the flowing water away from the toe of the dam.

(6) Establish procedures and supervise backfilling of the embankment sections on either side of the stoplog spillway.

c. Within one year from the date of approval of this report the owner should engage a qualified professional consultant to design and supervise installation of adequate means to drain the reservoir in case of emergency.

d. Within thirty days from the date of approval of this report the following remedial actions should be initiated:

(1) Clear debris and trees from the spillway discharge channels and maintain the channels free from debris.

(2) Clear brush and uncontrolled vegetation from slopes of the dam and keep the slopes free from all debris.

(3) Clear trees and brush for some distance downstream from the toe of the dam and from the banks of the discharge channels for some distance downstream from the spillways.

e. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam, within one year from the date of approval of this report.

f. An emergency action plan and warning system should be developed which outlines actions to be taken by the owner to minimize the downstream effects of an emergency at the dam within six months from the date of approval of this report.

APPROVED:



ROGER L. BALDWIN

Lieutenant Colonel, Corps of Engineers
Commander and District Engineer

DATE:



PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM

Name of Dam:	Hope Lake
Identification No.:	Fed ID No. NJ00796
State Located:	New Jersey
County Located:	Warren
Stream:	Beaver Brook
River Basin:	Delaware
Date of Inspection	April 21, 1981

ASSESSMENT OF GENERAL CONDITIONS

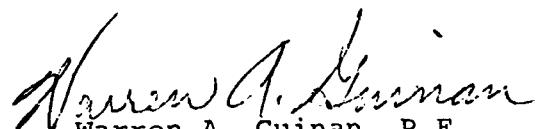
Hope Lake Dam is an earthfill, stone masonry, and concrete dam, about 200 years old, that is in poor overall condition. It is small in size and should be downgraded to significant hazard from its initial classification of high hazard. Trees and brush are growing on both upstream and downstream slopes of the earth embankment portions of the dam. One large tree has blown down causing a large hole in the downstream embankment where the roots were torn out near the left abutment of the principal spillway. Severe erosion of the embankments on either side of the stoplog spillway has undermined the concrete capping and exposed the concrete and stone masonry of the training walls. Much of the downstream stone masonry face under the concrete apron of the emergency spillway has collapsed leaving the slab unsupported. Erosion of the upstream slope at and above the waterline has occurred. Soft, wet areas were noted along the downstream toe of the embankment portions with some clear water discharges. The left abutment of the principal spillway has been patched; yet some leakage was noted below the patch. Leakage around the ends and through the stoplogs was observed. Also, seepage is occurring through the upstream concrete or stone masonry faces at both the stoplog and emergency spillways. The total combined capacities of the principal, emergency, and stoplog spillways (with stoplogs in place) can pass 4 percent of the one-half PMF without overtopping; thus the spillways are considered inadequate.

It is recommended that the owner retain the services of a professional engineer, qualified in the design and inspection of dams, to accomplish the following in the time periods specified. Starting immediately: investigate the cause of the seepage and wet, soft areas at the downstream toe of the dam; very soon: design procedures for and inspect the removal of the trees and their roots from the entire embankment; design procedures for and inspect the construction of erosion

protection on the upstream slope of the dam; design procedures for the repair or replacement of the gated and ungated spillways where considerable erosion and seepage are taking place; design channels to reroute the flowing water away from the toe of the dam; and establish procedures and supervise backfilling of the embankment sections on either side of the stoplog spillway. In the near future: further evaluate the hydrology and hydraulics of the watershed, reservoir, dam, spillways, and design and implement remedial measures; and design and install adequate means to drain the reservoir in case of emergency.

It is also recommended that, as a part of operating and maintenance procedures, the owner should immediately clear debris and trees from the spillway discharge channels and maintain the channels free from debris; check the condition of the dam periodically; clear brush and uncontrolled vegetation from slopes of the dam and keep the slopes free from all debris, and clear trees and brush for some distance downstream from the toe of the dam and from the banks of the discharge channels for some distance downstream from the spillways. In addition, in the future: establish a surveillance program for use during and immediately following periods of heavy rainfall and also a warning program to follow in case of emergency conditions.

ANDERSON-NICHOLS & COMPANY, INC.



Warren A. Guinan, P.E.
Project Manager
New Jersey No. 16848



21 April 1981

OVERVIEW
HOPE LAKE DAM

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test Flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonable possible storm runoff), or fractions thereof. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY INSPECTION PROGRAM
HOPE LAKE DAM
FED ID NO. #NJ00796

SECTION 1
PROJECT INFORMATION

5.1 General

a. Authority. Authority to perform the Phase I Safety Inspection of Hope Lake Dam was received from the State of New Jersey, Department of Environmental Protection, Division of Water Resources by letter dated 12 December 1980 under Basic Contract No. FPM-39 and Contract No. A01093 dated 10 October 1979. This Authority was given pursuant to the National Dam Inspection Act, Public Law 92-367 and by agreement between the State and the U.S. Army Engineers District, Philadelphia. The inspection discussed herein was performed by Anderson-Nichols & Company, Inc.

b. Purpose: The purpose of the Phase I Investigation is to develop an assessment of the general conditions with respect to the safety of Hope Lake Dam and appurtenances. Conclusions are based upon available data and visual inspection. The results of this study are used to determine any need for emergency measures and conclude if additional studies, investigations, and analyses are necessary and warranted.

1.2 Project Description

a. Description of Dam and Appurtenances. Hope Lake Dam is a 233-foot long 8.6-foot high earthfill, stone masonry, and concrete structure. The dam crest is approximately 12.5 feet wide with 2.5H:1V slope brush covered earthen embankment on the upstream side. The downstream embankment at Hope Lake Dam is tree covered with a 2H:1V slope. The dam crest is grass covered with small trees growing on it as well. The concrete capped, stone masonry principal spillway is located on the right side of the dam and is 60 feet long and 2 feet wide. A stoplog section is located approximately in the middle of the dam and consists of four 4"x 8" planks placed in a 4'x 4' bay. The concrete capped, stone masonry emergency spillway is located near the left abutment and is 52.4 feet long with a crest width of about 8 inches, it has a concrete slab apron upstream and a 6.5 foot downstream apron. At the end of the left abutment there is a small canal that is about 9 feet wide at the inlet, that formerly used to supply water power for a mill about a quarter mile downstream.

b. Location. Hope Lake Dam is located on Beaver Brook in Hope Township, Warren County, New Jersey. The Dam is at 40° 54.5' north latitude 74° 58.0' west longitude on the Blairstown Quadrangle. A location map has been included as Figure 2. The dam can be reached by taking exit 12 off Rt. 80 west, onto Rt. 521 south. The dam is on the left a mile from the Rt. 521 exit.

c. Size Classification. Hope Lake Dam is classified as being small in size on the basis of storage at the top of dam of 100 acre-feet, which is less than 1000 acre-feet but more than 50 acre-feet, and on the basis of its structural height of 8.8 feet, which is less than 40 feet, in accordance with criteria given in the Recommended Guidelines for Safety Inspection of Dams.

d. Hazard Classification. Visual inspection of the area below Hope Lake Dam indicated that a single house of about 0.1 mile downstream on the left bank could have up to 6 feet of flood water in the garage beneath the house from either overtopping or breaching of the dam. About two feet of overtopping of the road crossings downstream of the house, would likely result in considerable property damage and possible loss of life. For these reasons, the dam is given a significant hazard classification.

e. Ownership. The dam is owned by Mr. & Mrs. Charles Southwick, P.O. Box 282, Milbrook Road, Hope, New Jersey; for information they may be reached at the above address.

f. Purpose. The original purpose of Hope Lake Dam was to generate power for the downstream mill; recreation is its present purpose.

g. Design and Construction History. No information regarding the original plan or design of the dam was available. Mrs. Southwick said that the dam was originally built by Moravians about 1769. The mill race was dug out by hand using adzes.

h. Normal Operational Procedure. No operational procedures exist for the dam.

i. Site Geology. No site specific geologic information (such as borings) was available at the time the dam was inspected. Information derived from the Geologic Map of New Jersey (Lewis and Kummel, 1912) and Glacial Drift Map of New Jersey (Kummel and Peet, 1902) indicates that the soils within the immediate site area consist of stratified glacial deposits in the form of sands and gravels, deltas, eskers, kames, and terraces.

The depth to bedrock at the dam site is unknown. From the reports previously mentioned, bedrock in this area consists of massive to thin bedded limestones which are Cambrian to Ordovician in age. However, bedrock exposure in the 16-foot cut for the mill race is a dark, fissile, steeply dipping shale. This exposure is about 200 feet downstream of the dam.

1.3 Pertinent Data

a. Drainage Area

7.7 square miles

b. Discharge at Damsite (cfs)

Maximum flood at damsite - unknown.

Total ungated spillway capacity at maximum elevation - 337 (with stoplogs in place)

c. Elevation (ft. above NGVD)

Top of dam - 426.0

Maximum pool design surcharge (1/2 PMF) - 430.3

Recreation pool (at time of inspection) - 424.9

Spillway crest - 424.7

Streambed at centerline of principal spillway - 420.4

Maximum tailwater (estimated) - 422.8
(10 ft downstream of dam)

d. Reservoir (feet)

Length of maximum pool - 2600 (estimated)

Spillway crest - 1800

e. Storage (acre-feet)

Spillway crest - 64

Design surcharge (1/2 PMF) - 725

Top of dam - 100

f. Reservoir Surface (acres)

Top of dam - 25 (estimated)

Spillway crest - 12.8

g. Dam

Type - earthfill, stone masonry, and concrete

Length - 233 feet

Height - 8.6 feet (hydraulic)

- 8.8 feet (structural)

Top width - 12.5 feet

Side slopes - upstream 2.5 H:1V, downstream 2H:1V

Zoning - unknown

Impervious core - unknown

Cutoff - unknown

Grout curtain - unknown

h. Principal Spillway

Type - Concrete capped stone masonry

Length of weir - 60

Crest elevation - 424.7 feet NGVD

Low level outlet - none

U/S channel - Hope Lake

D/S channel - Beaver Brook

i. Emergency Spillway

Type - Concrete capping over stone masonry

Length of weir - 52.4

Crest elevation - 425.2

Gates - none

U/S channel - Hope Lake

D/S channel - Beaver Brook

j. Stoplog Spillway

Type - 4"x8" wood planks (4.5 ft long)

Length of weir - 4 feet

Crest elevation - 425.6 (with stoplogs) 421.6 (without stoplogs)

U/S channel - Hope Lake

D/S channel - Beaver Brook

SECTION 2
ENGINEERING DATA

2.1 Design

No original plans, hydraulic or hydrologic data for Hope Lake Dam were available.

2.2 Construction

No data concerning the original construction of Hope Lake Dam were revealed; however, owner indicated that it was built over 200 years ago.

2.3 Operation

No data pertaining to the operation of the dam were found.

2.4 Evaluation

- a. Availability. A search of the New Jersey Department of Environmental Protection Files and contact with representatives of the owner of the dam revealed no pertinent information.
- b. Adequacy. Evaluation was based primarily on visual observations and measurements which were adequate for this study.

SECTION 3
VISUAL INSPECTION

3.1 Findings

a. Dam. The area at the downstream toe of the dam is generally wet and soft and some clear seepage water is discharging. Trees are growing on the upstream slope, crest, on the downstream slope and in the area at the downstream toe of the dam. A large tree has been uprooted from the crest near the spillway at the right abutment and its root ball has been pulled out, leaving a large hole on the crest. Roots of trees were observed extending from the upstream slope near the water line toward the downstream edge of the crest.

The crest of the dam is partially covered with grass with a pedestrian path extending along the entire length. Considerable erosion has taken place on the upstream slope at and above the water line. The downstream slope has undergone considerable erosion and slumping adjacent to each of three spillways. In addition, erosion has occurred along portions of the toe that is due to water passing over the spillways and flowing adjacent to the toe in the discharge channels.

b. Appurtenant Structures.

(1) Ungated emergency spillway - left end. The concrete weir is badly eroded and irregular, and the downstream dry stone masonry wall has collapsed in several areas undermining the concrete apron. The entrance to the spillway is partially clogged with wood and grass vegetation. The left training wall is cracked and has settled approximately 1.5 inches.

(2) Gated spillway - middle of dam. The concrete walls and sill of the stoplog facility are badly eroded and spalled. Considerable undermining has occurred around the abutments of the spillway walls. An attempt to reduce erosion and seepage using gunite, sand bags, concrete, concrete blocks, and bags of cement beneath and adjacent to the spillway has not been successful. The wood stoplog gate is deteriorated and is leaking around the ends and through the joints. The wooden bridge is also badly weathered. The concrete block, cast-in-place concrete and stone masonry walls on top of the dam extending right and left from the gated spillway are cracked, irregular, and show considerable leakage on both sides. The downstream face is badly eroded and undermined on both sides of the spillway.

(3) Ungated principal spillway - right end. The crest of the spillway is cracked and eroded, and the downstream face is badly spalled causing undermining of the spillway. Seepage was noted near the left end of the spillway where the original crest had been repaired for about 5 feet from the left abutment of the spillway with stones and concrete.

c. Reservoir Area. The watershed above the lake is gently sloping and wooded. Some open fields exist along the west side of the reservoir. Slopes on the shore of the lake appear to be stable. Evidence of significant sedimentation was observed.

d. Downstream Channel. Considerable erosion has occurred on the right and left bank of each channel immediately downstream of the spillways for a distance of approximately 100 to 150 feet. Trees are growing on the banks of the channels and within the confines of the channels.

SECTION 4
OPERATIONAL PROCEDURES

4.1 Procedures

No formal operating procedures were revealed.

4.2 Maintenance of Dam

No formal maintenance procedures for the dam were found.

4.3 Maintenance of Operating Facilities

No formal maintenance procedures for the operating facilities were discovered.

4.4 Warning System

No description of any warning system was found.

4.5 Evaluation of Operational Adequacy

Because of the lack of operation and maintenance procedures, the remedial measures described in Section 7.2 should be implemented as described.

SECTION 5 HYDROLOGIC/HYDRAULIC

5.1 Evaluation of Features

- a. Design Data. Because no data were revealed an evaluation of the hydrologic/hydraulic data could not be performed.
- b. Experience Data. No experience data were found.
- c. Visual Observation. Erosion at left abutment of the principal spillway has been patched with stones (6"-8") and mortar. This area shows some leakage. The crest of the emergency spillway shows considerable spalling. The stone masonry beneath the emergency spillway slab apron has fallen along the downstream face leaving much of the slab without support. Water is leaking through the stone masonry (estimate about 5 to 10 gpm). The stoplog spillway training walls are structurally in poor condition. The stoplog notches are eroded with leakage around the ends and between the logs. The dam has no other low level outlet.
- d. Hope Lake Overtopping Potential. The hydraulic/hydrologic evaluation for the dam is based on a selected Spillway Design Flood (SDF) equal to one-half the Probable Maximum Flood (PMF) in accordance with the range of test floods given in the evaluation guidelines, for dams classified as significant hazard and small in size. The PMF was determined by application of a 24-hour probable maximum storm of 23.1 inches to the SCS dimensionless unit hydrograph. Hydrologic computations are given in Appendix 3. The routed one-half PMF peak discharge for the subject drainage area is 8,385 cfs.

The minimum elevation of the dam allows 1.3 foot of depth above the principal spillway, 0.8 foot above the emergency spillway and 0.4 foot above the stoplog spillway (with stoplogs in place) before overtopping occurs. Under this head the total spillway capacity for the 3 spillways is 337 cfs, which is less than the selected SDF (approximately 4 percent).

At discharges above 6900 cfs, the backwater resulting from the narrowing and gradual slope of the channel downstream of the dam begins to cause slightly less flow over the dam than would occur without this backwater effect. Because this effect was found to be negligible for Hope Lake Dam, the discharge coefficient for the spillway weir was not changed. Calculations are shown in Appendix 3.

Flood routing calculations indicate that Hope Lake Dam will be overtopped for 13.2 hours to a maximum depth of 4.3 feet under one-half PMF conditions. It is estimated that the principal spillway can pass 2 percent (240 cfs) of the one-half PMF without overtopping the dam; thus, the spillway is considered inadequate.

3. Drawdown Capacity. There are no drawdown pipes for Hope Lake Dam.

SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

a. The soft, wet areas and seepage at the downstream toe of the dam is indicative of seepage through and under the dam, which, if not properly controlled, could lead to failure of the dam by piping or sloughing of the downstream slope. Trees growing on the crest and on the upstream and downstream slopes may cause seepage and erosion problems if a tree blows over and pulls out its roots, or if a tree dies or is cut and its roots rot. One large tree has already blown over, leaving a hole in the crest where its roots pulled out and this hole weakens the crest. Erosion at the abutments of the spillways and seepage below and adjacent to these structures could lead to breaching of the dam at these locations if not controlled. Erosion caused by overtopping of the upstream concrete walls on either side of the center spillway could lead to breaching.

Erosion of the upstream slope at the water line could eventually lead to breaching of the dam.

6.2 Design and Construction Data. No design or construction data pertinent to the structural stability of the dam are available.

6.3 Operating Records. No operating records pertinent to the structural stability of the dam were available.

6.4 Post-Construction Changes

No record of post-construction changes was available. However, evidence of numerous patchings are clearly visible.

6.5 Seismic Stability - This dam is in Seismic Zone 1. According to the Recommended Guidelines, dams located in Seismic Zone 1 "may be assumed to present no hazard from earthquake provided static stability conditions are satisfactory and conventional safety margins exist." None of the visual observations made during the inspection are indicative of unstable slopes. However, because no data are available concerning the engineering properties of the embankment and foundation materials for this dam, it is not possible to make an engineering evaluation of the stability of the slopes or the factor of safety under static conditions.

SECTION 7
ASSESSMENT, RECOMMENDATIONS/REMEDIAL MEASURES

7.1 Dam Assessment

- a. Condition. Hope Lake is probably over 200 years old and is in very poor condition.
- b. Adequacy of Information. The information available is such that the assessment of the dam must be based entirely on the results of the visual inspection.
- c. Urgency. The recommendations made in 7.2.a and 7.2.b should be implemented by the owner as prescribed.
- d. Necessity for Additional Data/Evaluation. The information available from the visual inspection is adequate to identify the potential problems which are listed in 7.2.a. These problems require the attention of a professional engineer who will have to make additional engineering studies to design or specify remedial measures to rectify the problems. If left unattended, the problems could lead to failure of the dam.

7.2 Recommendation/Remedial Measures

a. Recommendations

The owner should retain a professional engineer qualified in the design and construction of dams to accomplish the following in the time periods specified:

Immediately:

Investigate the cause of the seepage and wet, soft areas at the downstream toe of the dam.

Very soon:

- (1) Design procedures for and inspect the removal of the trees and their roots from the entire embankment.
- (2) Design procedures for and inspect the construction of erosion protection on the upstream slope of the dam.
- (3) Design procedures for the repair or replacement of the gated and ungated spillways where considerable erosion and seepage are taking place.

- (4) Design channels to reroute the flowing water away from the toe of the dam.
- (5) Establish procedures and supervise backfilling of the embankment sections on either side of the stoplog spillway.

In the near future:

- (1) Further evaluate the hydrology and hydraulics of the watershed, reservoir, dam, and spillways, and design and implement necessary mitigating measures. Items b(2) and b(3) following should be considered in conjunction with this recommendation.
- (2) Design and install adequate means to drain the reservoir in case of emergency.

b. Operating and Maintenance Procedures

The owner should do the following immediately:

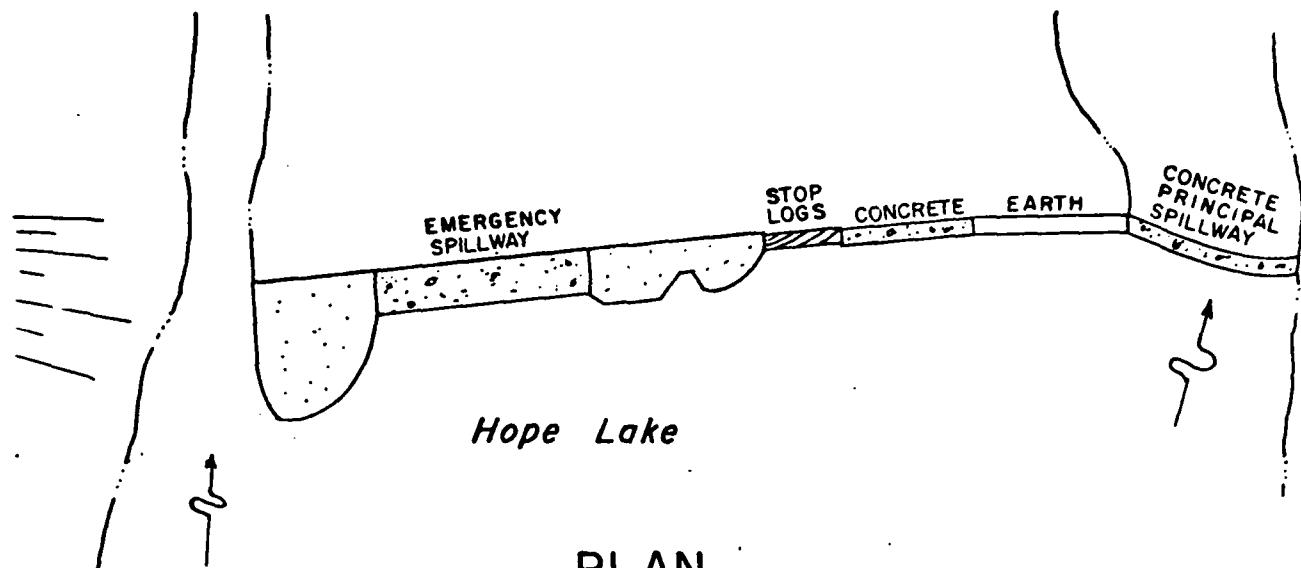
- (1) Clear debris and trees from the spillway discharge channels and maintain the channels free from debris.
- (2) Check the condition of the dam periodically.
- (3) Clear brush and uncontrolled vegetation from slopes of the dam and keep the slopes free from all debris.
- (4) Clear trees and brush for some distance downstream from the toe of the dam and from the banks of the discharge channels for some distance downstream from the spillways.

In the near future:

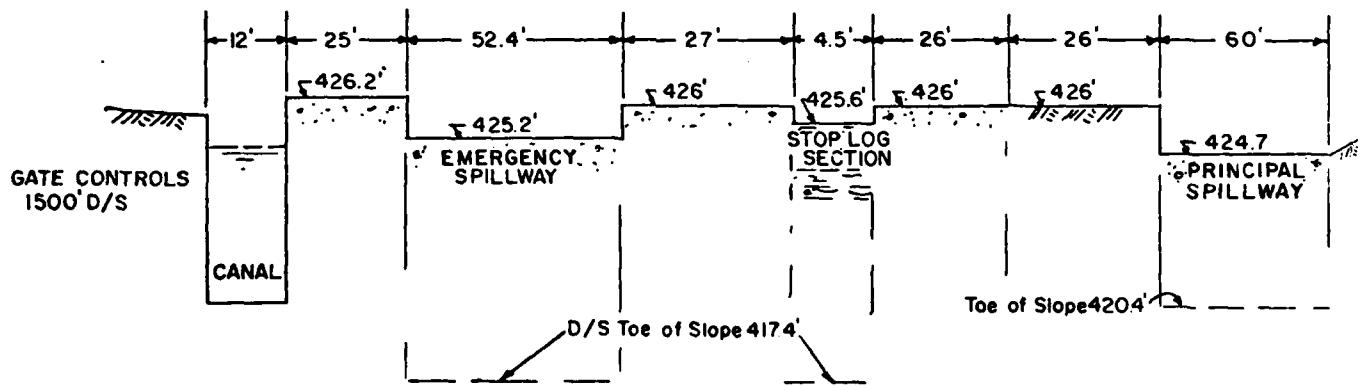
Develop written operation procedures and a periodic maintenance plan to ensure the safety of the dam.

In the future:

Establish a surveillance program for use during and immediately following periods of heavy rainfall and also a warning program to follow in case of emergency conditions.



PLAN



ELEVATION

Anderson-Nichols & Co, Inc BOSTON		U.S. ARMY ENGINEER DIST PHILADELPHIA CORPS OF ENGINEERS PHILADELPHIA, PA	
NATIONAL PROGRAM OF INSPECTION OF NON-FED.DAMS			
HOPE LAKE DAM			
BEAVER BROOK		NEW JERSEY	
		SCALE NOT TO SCALE	
		DATE MAY 1981	
FIGURE 1			



SCALE IN MILES

Anderson-Nichols & Co., Inc.

MASSACHUSETTS

U.S. ARMY ENGINEER DIST. PHILADELPHIA
CORPS OF ENGINEERS
PHILADELPHIA, PA.

NATIONAL PROGRAM OF INSPECTION OF NON-FED DAMS

• HOPE LAKE DAM LOCATION MAP

BEAVER BROOK

NEW JERSEY

SCALE: 1" = 4 Miles APPROX.
DATE: MAY 1981

**MAP BASED ON STATE OF NEW JERSEY
OFFICIAL MAP & GUIDE.**

APPENDIX 1

CHECK LIST

VISUAL INSPECTION

HOPE LAKE DAM

Check List
Visual Inspection
Phase 1

Name Dam	Hope Lake (NJ00796)	County	Warren	State	New Jersey	Coordinators	NJDEP
Date(s) Inspection	2/16/81		Fair, clear				36°
	4/22/81	Weather	Clear, cold		Temperature		38°
Pool Elevation at Time of Inspection	424.9	NGVD	Tailwater at Time of Inspection	418.2	NGVD		

Inspection Personnel:

W. Guinan	S. Gilman
J. Stone	R. Murdock

Guinan/Gilman Recorder

Mrs. Charles Southwick, owner, was present with the inspection party.

UNGATED SPILLWAY
Right End of Dam

VISUAL EXAMINATION OF

REMARKS OR RECOMMENDATIONS

OBSERVATIONS

CONCRETE WEIR

Concrete weir is curved. Top surface is eroded and cracked. Right ends show evidence of movement. Downstream face is badly eroded and spalled undermining face and bottom of wall. Left end has been repaired with mortared cobbles- 6-8 in +. Seepage and leakage noted at both ends of spillway.

DISCHARGE CHANNEL

Under water, appears to be shallow, unobstructed.

BRIDGE AND PIERS
OVER SPILLWAY

None

Clear trees and brush 25 ft on either side of discharge channel for a distance of 100 ft downstream from the dam or to the property line, whichever is less.

Stop Log Section and Adjacent Concrete Dam

GATED SPILLWAY
at Center of Dam

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONCRETE SILL	Bottom of stop log section is eroded & deteriorated in <u>+</u> .	Major construction required of entire structure.
APPROACH CHANNEL	Upstream face of stop log section is badly deteriorated with concrete cap showing evidence of forward movement.	
DISCHARGE CHANNEL	Sidewalls are badly cracked and spalled. Some repairs have been made with mortared stone.	Clear trees and brush 25 ft on either side of discharge channel for a distance of 100 ft downstream from the dam.
BRIDGE AND PIERS	2 in wood planks are badly weathered with some deterioration.	See note above Major Construction
GATES AND OPERATION EQUIPMENT	Stop logs are deflected. All planks show evidence of deterioration. Leakage is observed around ends of stop log and thru joints. Stop log slots are badly eroded.	See note above Major Construction
CONCRETE DAM WALLS ADJACENT TO GATED SPILLWAY	Walls are cracked, irregular and show considerable leakage on both sides. D/S face is badly eroded and undermined on both sides.	See note above Major Construction

UNGATED SPILLWAY
Left End of Dam

VISUAL EXAMINATION OF

OBSERVATIONS

REMARKS OR RECOMMENDATIONS

CONCRETE WEIR
The top of the concrete weir is badly eroded and uneven. D/S apron is in fair condition. Left training wall is cracked and has settled 1.5 in. Dry stone masonry wall on d/s face has collapsed in several areas.

Repair concrete weir. Repair dry stone masonry wall.

APPROACH CHANNEL

Under water, appears to be shallow, unobstructed.

DISCHARGE CHANNEL

Debris, fallen trees, boulders in bottom channel, joins with discharge channel for gated spillway.

Clear trees and brush 25 ft on either side of discharge channel for a distance of 100 ft downstream from the dam or up to the property line, whichever is less.

BRIDGE AND PIERS
OVER SPILLWAY

None.

EMBANKMENT

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS	None observed.	
UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE	None apparent.	
SLoughing OR Erosion OF EMBANKMENT AND ABUTMENT SLOPES	Pronounced erosion on both upstream and downstream slopes. Trees present on both slopes.	Control trespassing on dam. Repair erosion on dam.
VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST	Horizontal alignment - fair. Vertical alignment - right undulation of crest.	
RIPRAP FAILURES	Slight amount of riprap evident below water surface. Only a few riprap pieces present on the slope.	

EMBANKMENT

VISUAL EXAMINATION OF

	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
RAILINGS	None apparent.	
JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM	Erosion at both abutments and at junction with spillway structure. See Notes in "Ungated Spillway" regarding concrete walls along embankment.	Investigate seepage and design appropriate remedial measures.
ANY NOTICEABLE SEEPAGE	Seepage evident below and adjacent to spillway, emergency spillway and gated spillway.	
STAFF GAGE AND RECORDER	None apparent.	
DRAINS	None apparent.	

INSTRUMENTATION

VISUAL EXAMINATION	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
MONUMENTATION/SURVEYS	None apparent.	
OBSERVATION WELLS	None apparent.	
WEIRS	None apparent.	
PIEZOMETERS	None apparent.	
OTHER	None apparent.	

RESERVOIR

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SLOPES	Gradual slopes, wooded. Open fields.	
SEDIMENTATION	Appears to be significant sedimentation in the reservoir.	

DOWNSTREAM CHANNEL

VISUAL EXAMINATION OF CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
Debris, boulders in channel: Banks heavily overgrown with trees and vines.		
SLOPES	Trees and brush covered, gentle slopes on the right bank; tree- and brush-covered steep slopes with a flat flood plain on the left bank.	
APPROXIMATE NO. OF HOMES AND POPULATION		One house about 0.1 mile downstream on left bank with 2 residents. The first floor is about 14 feet above the channel invert. Three empty buildings (corn canning plant) on the right bank are within 100 yards of the dam with a first floor elevation from 8 to 10 ft above channel bottom.

CHECK LIST
ENGINEERING DATA
DESIGN, CONSTRUCTION, OPERATION

ITEM	REMARKS
PLAN OF DAM	None found
REGIONAL VICINITY MAP	Prepared for this report
CONSTRUCTION HISTORY	None found
TYPICAL SECTIONS OF DAM	None
HYDROLOGIC/HYDRAULIC DATA	None
OUTLETS - PLAN	None found
- DETAILS	None found
- CONSTRAINTS	None found
- DISCHARGE RATINGS	None found
RAINFALL/RESERVOIR RECORDS	None found

ITEM		REMARKS
DESIGN REPORTS	None found	
GEOLOGY REPORTS	None found	
DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS DAM STABILITY SEEPAGE STUDIES	None found	
MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD	None found	
POST-CONSTRUCTION SURVEYS OF DAM	None found	
BORROW SOURCES	Unknown	

ITEM	REMARKS
MONITORING SYSTEMS	None
MODIFICATIONS	None
HIGH POOL RECORDS	None
POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS	None
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	None
MAINTENANCE OPERATION RECORDS	None

ITEMS	REMARKS
SPIIWAY PLAN	Prepared for this report from field inspection
SECTIONS	None
DETAILS	None
OPERATING EQUIPMENT PLANS & DETAILS	None

CHECK LIST
HYDROLOGIC AND HYDRAULIC DATA
ENGINEERING DATA

DRAINAGE AREA CHARACTERISTICS: 7.7 square miles, gentle slope, woods.

ELEVATION TOP NORMAL POOL (STORAGE CAPACITY): 424.7' NGVD
(64 acre-feet).

ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY)
Not applicable

ELEVATION MAXIMUM HIGH POINT ON DAM: 426.2' NGVD

ELEVATION TOP DAM: 426.0' NGVD

PRINCIPAL SPILLWAY CREST: Uncontrolled concrete capped stone
masonry

a. Elevation 424.7' NGVD

b. Type Concrete

c. Width 2 feet

d. Length 60 feet

e. Location Spillover Right end of dam

f. Number and Type of Gates None

EMERGENCY SPILLWAY CREST: Free overflow concrete spillway

a. Elevation 425.2' NGVD

b. Type Concrete

c. Width 12.5 feet w/aprons up and downstream

d. Length 52.4 feet

e. Location Spillover Left of center of dam

f. Number and Type of Gates None

STOPLOG SECTION: 4" x 8" wood planks

- a. Elevation 426.5" NGVD
- b. Type Wood planks
- c. Width 4 inches
- d. Length 4.5 feet
- e. Location Spillover Center of dam
- f. Number and Type of Gates Four 4" x 8" stoplogs

OUTLET WORKS: None

HYDROMETEOROLOGICAL GAGES: None

MAXIMUM NON-DAMAGING DISCHARGE: 337 cfs (Total spillway capacity)

APPENDIX 2

PHOTOGRAPHS

HOPE LAKE DAM



21 April 1981

Spillway crest looking toward left (east) side of dam



21 April 1981

Looking eastward across emergency spillway crest and apron



21 April 1981

View of downstream face of emergency spillway



21 April 1981

Looking u/s at stoplog spillway



21 April 1981

View of undermining of concrete cap on stoplog spillway training wall.



21 April 1981

Outside and d/s appearance of right training wall of stoplog spillway



18 February 1981

Looking u/s across Hope Lake Reservoir



21 April 1981

Spillway channel looking downstream

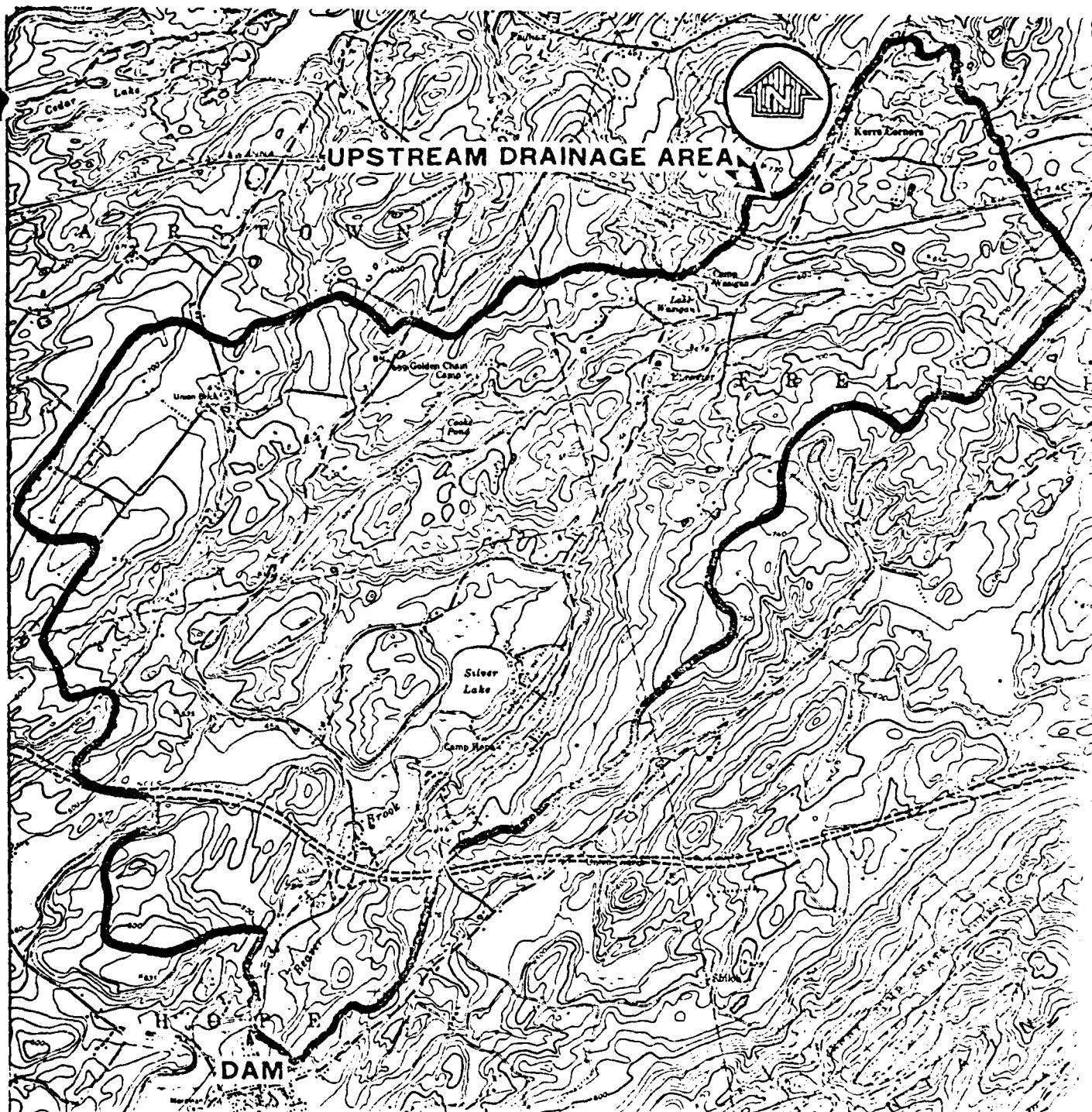


21 April 1981

Mill Race looking d/s near left (east) end of dam

APPENDIX 3
HYDROLOGIC COMPUTATIONS

HOPE LAKE DAM



NATIONAL PROGRAM OF INSPECTION OF
NON-FED. DAMS

HOPE LAKE DAM
HOPE TOWNSHIP, NEW JERSEY

REGIONAL VICINITY MAP
MAY 1981

DEPARTMENT OF THE ARMY
PHILADELPHIA DISTRICT, CORPS OF ENGINEERS
PHILADELPHIA, PENNSYLVANIA

SCALE IN MILES

0 1/2

MAP BASED ON U.S.G.S. 7.5 MINUTE QUADRANGLE
SHEET. BLAIRSTOWN, N.J. 1954, REVISED 1971.

JOB NO.

SQUARES
1/4 IN. SCALE

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29

1 **TIME OF CONCENTRATION**2 **① Texas Highway Method**3 **Overland**4 **woodlands**5 **reach = 5000'**

6
$$7 \text{slope} = \frac{734 - 600}{5000} = 0.027$$

8
$$9 \text{ave vel} = 1 \text{ fps} \quad \frac{2000 \text{ ft}}{1 \text{ ft/sec}} = 6000 \text{ sec}$$

$$10 = 83 \text{ min} = 1.4 \text{ hrs.}$$

11 **Channel**12 **reach = 25,000'**

13
$$14 \text{slope} = \frac{600 - 435}{25,000} = .007$$

15
$$16 \text{ave vel} = 2 \text{ fps} \quad \frac{25000'}{1 \text{ sec}} = 12500 \text{ sec}$$

$$17 = 208 \text{ min} = 3.5 \text{ hrs}$$

18
$$19 \text{TOTAL } t_C = 1.4 + 3.5 = 4.9 \text{ hrs}$$

20 **② Soil & Water Conservation**

21
$$22 L = \frac{P^{0.8} (S+1)^{1.67}}{9000 Y^{0.5}} \quad 23 \text{CN} = \frac{P^{0.8} (S+1)^{1.67}}{9000 Y^{0.5}} - 10$$

24
$$25 L = 5000 + 25000 = 30,000'$$

26
$$27 \text{CN} = 70 \text{ for } L = 30,000'$$

28
$$29 S = \frac{1000}{70} - 10 = 6.1$$

30
$$31 Y = \frac{0.027 + 0.007}{2} = 0.017 = 1.7\%$$

JOB NO.

SQUARES
1/4 IN. SCALE 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30

$$L = \frac{(30,000)^{0.8} (4.3+1)^{1.67}}{9000 (17)^{0.5}} = 5.2 \text{ hrs.}$$

$$T_c = \frac{L}{6} = \frac{5.2}{6} = \underline{\underline{8.7 \text{ hrs}}}$$

(3) SCS TR #55 method

overland

$$l = 5,000 \text{ head} = 134'$$

$$\text{slope} = 0.027 \quad \text{woodland}$$

from plot of % slope vs. velocity, $V = 4 \text{ fps}$

$$\frac{5000 \text{ ft}}{4 \text{ ft/sec}} = 1250 \text{ sec} = 03.5 \text{ hrs}$$

channel

$$l = 25,000' \quad \text{slope} = 0.007 \quad n = .03$$

$$V = \frac{1.49}{n} R^{2/3} S^{1/2}$$

(assume 1' x 10' rectangular channel to calculate R)

$$R = \frac{A}{wP} = \frac{10}{2(10) + 10} = 0.83 \text{ ft}^2$$

$$V = \frac{1.49}{.03} (0.83)^{2/3} (.007)^{1/2} = 3.7 \text{ ft/sec}$$

$$\frac{25000 \text{ ft}}{3.7 \text{ ft/sec}} = 6793 \text{ sec} = 1.9 \text{ hrs}$$

$$\text{TOTAL} = 1.9 + 3.5 = \underline{\underline{5.4 \text{ hrs}}}$$

JOB NO.

SQUARES 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29

(4) Kerby Method

$$T_c = 0.83 \left(\frac{Nl}{\sqrt{s}} \right)^{0.467}$$

$$l = 5000' \quad s = .027 \quad N = 0.60$$

$$T_c = 0.83 \left[\frac{(0.6)(5000)}{\sqrt{.027}} \right]^{0.467} = \underline{1.4 \text{ hrs}}$$

for channel use

Manning's, as Method 3

$$V = 3.6 \text{ f/s} \quad \frac{25 \text{ acre ft}}{3.6 \text{ ft/sec}} = 6944 \text{ sec} = \underline{1.9 \text{ hrs.}}$$

$$T_c = 1.4 + 1.9 = \underline{3.3 \text{ hrs.}}$$

$$\text{ave } T_c = \frac{4.9 + 8.7 + 5.4 + 3.3}{4} = 5.6 \text{ hrs}$$

$$T_{lag} = 0.6 \times 5.6 = \underline{3.3 \text{ hrs}}$$

X

JOB NO.

SQUARES 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30

1

2

STAGE - STORAGE DETERMINATIONS

3

4

ASSUME DEPTH OF LAKE TO BE 5 FEET

5

Elevation	Surface Area Acres	AVG SA. Acres	Incremental Storage Ac-Ft	Cumulative Storage Ac-Ft
424.7	12.8	12.8	64	64
440	345.6	176	2692.8	2756.8
460	614.4	480	9600	12356.8

6

7

8

9

10

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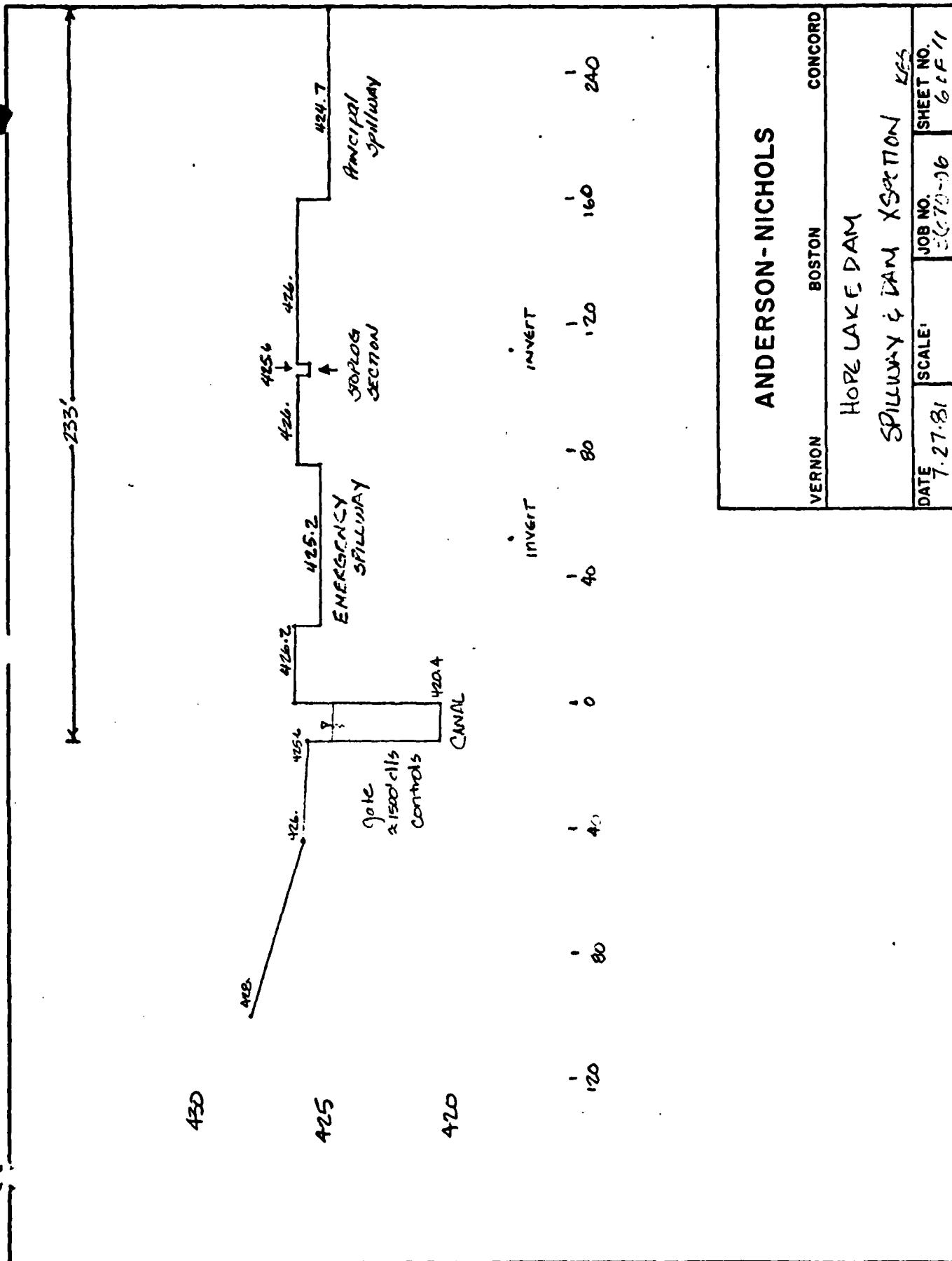
39

Input for Hec-I (from curve)

Stage	Storage
434.0	0
434.1	64
434.2	70
434.6	85
435.0	110
435.2	115
435.5	120
436.0	520
437.0	850
435.0	1500
440.0	2757

A graph on grid paper showing a downward-sloping curve. The vertical axis is labeled "HOTEL RATE DOLLARS" and the horizontal axis is labeled "FREQUENCY". The curve starts at approximately (10, 440) and ends at approximately (50, 150). A diagonal line is also drawn from (10, 440) to (50, 150).

FREQUENCY	HOTEL RATE DOLLARS
10	440
20	330
30	220
40	110
50	150



ANDERSON-NICHOLS

VERNON BOSTON CONCORD

HOPE LAKE DAM

SPILLWAY & DAM SECTION

DATE: 7.27.81 SCALE: 1:670-16 JOB NO. E-70-16 SHEET NO. 6 of 11

Anderson-Nichols & Company, Inc.

Subject Hope Lake

Sheet No. 7 of 11
Date 5/11/51
Computed CLF
Checked KCZ

JOB NO.

SQUARES 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30
1/4 SCALE

DEVELOPMENT OF RATINGS CIRCUIT

$$Q = C l \cdot H^{3/2}$$

① Spillway Closure

$$c = 2.7 \quad L = 60 \quad \text{width} = 2.0$$

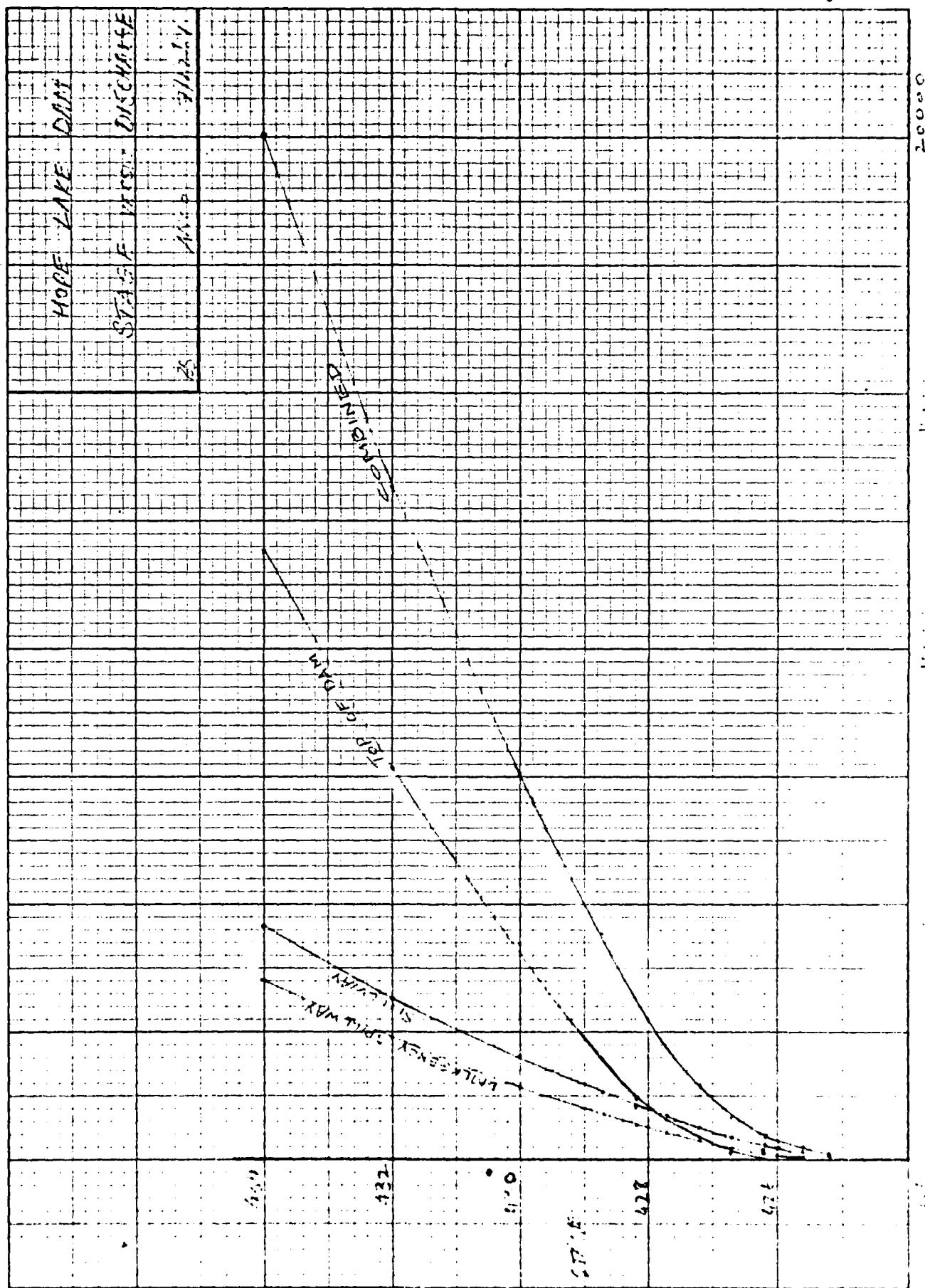
② Top of dam curve

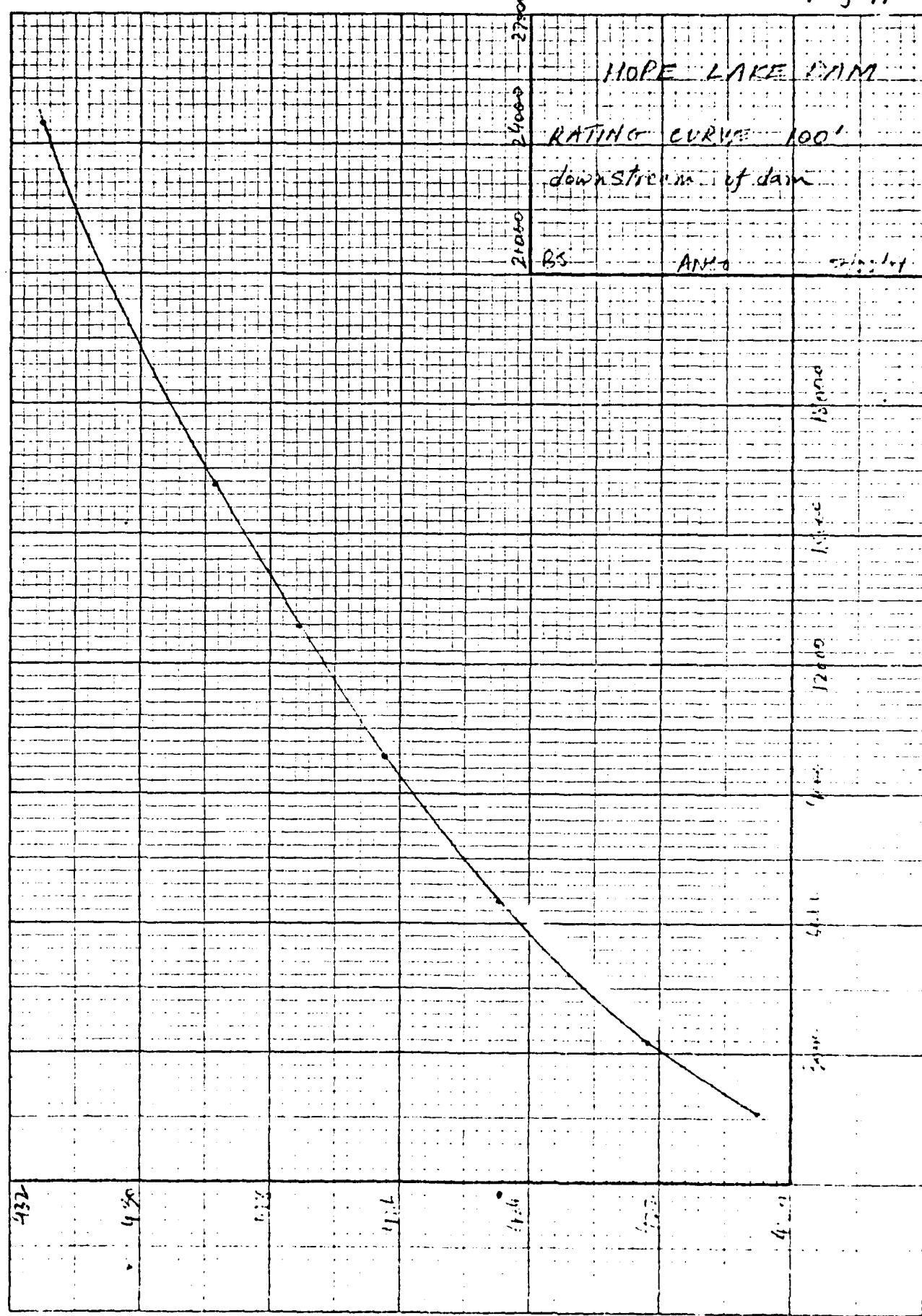
$$c = a \cdot b \quad L = 153^{\circ} \quad \text{width} = 12.5$$

③ Emergency Spillway

$$C=2.6 \quad L=52 \quad \text{width} = 6.5$$

12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	Elevation	Principal spillway		Emergency spilling		Top of Dam			Combined
		head	Q	head	Q	head	length	Q	
0.001	424.7	0		0					0
emer gency	425.2	0.5	57.2	0					57
stop page	425.6	1.0	162	0.5	18				210
TOP DAM	426.0	1.3	240	0.8	97				337
	426.2	1.5	298	1.0	135		153	140	433
	426.7	2.0	459	1.5	248	0.5	153	140	246
	427.2	2.5	540	2.0	332	1.0	170	442	442
	427.7	3.0	842	2.5	534	1.5	170	312	2193
	428.2	3.5	1061	3.0	701	2.0	190	1153	1153
	428.7	4.0	1276	3.5	934	2.5	190	1153	4133
	430.0	5.3	1777	4.3	1420	3.8	210	4045	7442
	432.0	7.3	3195	6.9	2314	5.9	210	7627	16216
	434.0	9.3	4595	8.3	3524	7.9	210	11314	20.013





JOB NO.

Weir Submergence Calculations

SQUARES
1/4 IN. SCALE 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30

1
2 Data for Rating Curve @ 100' downstream
3
4 from HEC-1
5

6 1 FLOW 1646. 3223. 6477. 9782. 12868. 16137. 24513. 33009.
7 TIME 19.67 19.83 19.75 19.75 19.83 19.83 19.75 19.67

8 ** PEAK STAGES IN FEET **

9 1 STAGE 420.52 422.16 424.45 426.22 427.57 428.82 431.46 433.66.
10 TIME 19.67 19.83 19.75 19.75 19.83 19.75 19.67 19.67

11 FROM HEC-1 CALCULATIONS -

12 $\frac{1}{2}$ PMF $Q = 8114 \text{ CFS}$

13 $\frac{1}{2}$ PMF ELEVATION d/s Xsect. = 425.9'

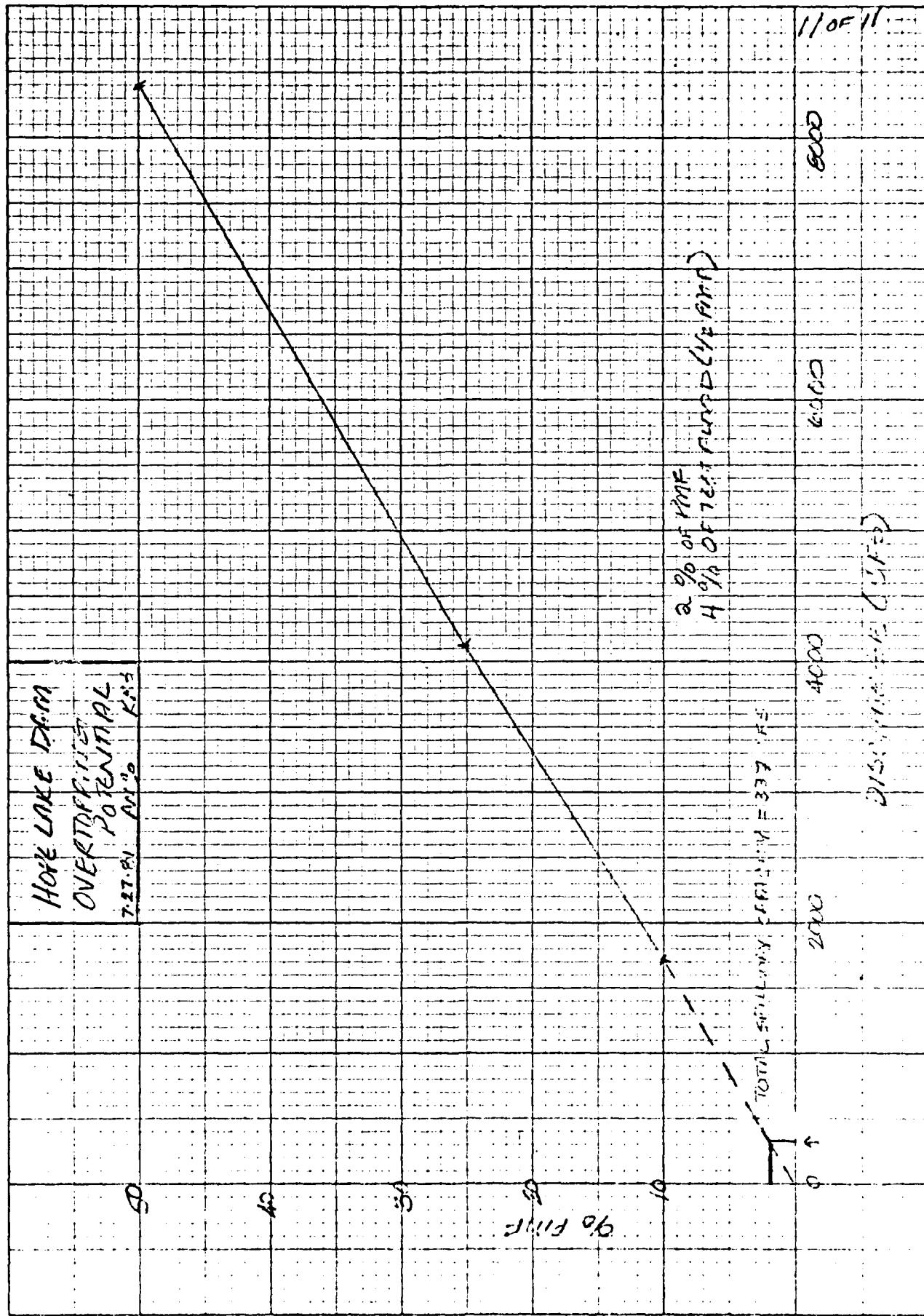
14 $\frac{1}{2}$ PMF ELEVATION dam = 431.2'

15 Calculations of decrease in discharge coefficient
16 for submerged orifices (spillway) (using Chow, 1959)
17 Chow's Open Channel Hydraulics, 1959



Q	Revised Xsect	Revised d	% Change	h_d	He	d	h_f	h_f
8114	425.9	431.2	1.2	5.3	6.5	9.7	0.6	1.2

0.23% reduction in 'C' value for weir (using Chow) - neglect



APPENDIX 4
HEC-1 OUTPUT
HOPE LAKE DAM

MFCC-1 Input

FILED AT FEDERAL BUREAU OF INVESTIGATION
FBI - WASHINGTON, D.C.
MURKIN, DATE 07/23/01 TIME 17.25.10
MEC-11

HOPE LAKE DAM NO. 796 - WARREN COUNTY, NEW JERSEY. OVERTOPPING ANALYSIS FROM 24-HOUR TOWNSHIP OF HOPE MULTIPLES OF PMF

5 10	OUTPUT CONTROL VARIABLES	PRINT CONTROL 2 PLOT CONTROL 1 PLOT SCALE 0 HYDROGRAPH PLOT SCALE YES PRINT DIAGNOSTIC MESSAGES
11	HYDROGRAPH TIME DATA	5 MINUTES IN COMPUTATION INTERVAL 1 DATE 1 000 STARTING DATE 1 TIME 0 300 NUMBER OF HYDROGRAPH ORDINATES 1 NO 2 0 0 ENDING DATE 1 NODATE 0 055 ENDING TIME

ENGLISH UNITS	SQUARE MILES
GRAINAGE AREA	INCHES
PRECIPITATION DEPTH	FEET
LENGTH.	CUBIC FEET PER SECOND
ELEVATION	ACRES FEET
STORAGE VOLUME	ACRES
SURFACE AREA	DEGREES FAHRENHEIT
TEMPERATURE	

MULTI-PLAN OPTION	M-PLAN	1	NUMBER OF PLANS
MULTI-RATIO OPTION	RATIOS OF RUNOFF	0.10 0.25	0.20

U.S. ARMY CIVIL ENGINEERING
INFRASTRUCTURE ENGINEERING CENTER
609 Second Street
DAVIS, CALIFORNIA 95616
(916) 440-3265 CR (FITS) 440-3265

U. S. ARMY CHURCH OF ENGLAND
THE HYBRIDIC CINELWING CHAPEL
909 ST. CLAIR STREET
DETROIT, MICHIGAN.

49161 U440-3285 (2 (FTS) 3285

PRECIPITATION DATA
 PROBABLE MAXIMUM 510.4 INEX PRECIPITATION
 4-HRS 23.5 COEFFICIENT
 TRSPC 0.80 TRANSPORTATION AREA
 16-HRS 2.70 TRANSPORTATION AREA
 SMD NO USE SWD DISTRIBUTION
 PERCENT OF INDEX PRECIPITATION OCCURRING IN GIVEN TIME
 6-HR 12-HR 12-HR 72-HR .96-HR
 112.0 132.0 132.0 0.0
 UNIFORM LOSS RATE
 STAB 1.00 INITIAL LOSS RATE
 CNST 0.10 UNIFORM LOSS RATE
 RTIMP 5.00 PERCENT IMPERVIOUS AREA
 SCS DIMENSIONLESS UNITGRAPH
 3.30 LAC

UNIT HYDROGRAPH TRUNCATED FROM 300 TO 150 INTERVALS

150 FNU OF HYDROGRAPH
UNIT-PERIOD-DIMINUTIVE
VOLUME = 1.00

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34
37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	
14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	1	2	3	4	
14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	1	2	3	4	

HYDROGRAPH AT STATION A1

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A decorative border consisting of a repeating pattern of small circles and dots. The pattern is composed of two rows of circles: a top row with larger circles and a bottom row with smaller circles. Between the rows are small black dots. The pattern is repeated horizontally across the entire width of the border.

1745	1750	1755	1760	1765	1770	1775	1780	1785	1790	1795	1800	1805	1810	1815	1820	1825	1830	1835	1840	1845	1850	1855	1860	1865	1870	1875	1880	1885	1890	1895	1900	1905	1910	1915	1920	1925	1930	1935	1940	1945	1950	1955	1960	1965	1970	1975	1980	1985	1990	1995	2000	2005	2010	2015	2020	2025	2030	2035	2040	2045	2050	2055	2060	2065	2070	2075	2080	2085	2090	2095	2100	2105	2110	2115	2120	2125	2130	2135	2140	2145	2150	2155	2160	2165	2170	2175	2180	2185	2190	2195	2200	2205	2210	2215	2220	2225	2230	2235	2240	2245	2250	2255	2260	2265	2270	2275	2280	2285	2290	2295	2300	2305	2310	2315	2320	2325	2330	2335	2340	2345	2350	2355	2360	2365	2370	2375	2380	2385	2390	2395	2400	2405	2410	2415	2420	2425	2430	2435	2440	2445	2450	2455	2460	2465	2470	2475	2480	2485	2490	2495	2500	2505	2510	2515	2520	2525	2530	2535	2540	2545	2550	2555	2560	2565	2570	2575	2580	2585	2590	2595	2600	2605	2610	2615	2620	2625	2630	2635	2640	2645	2650	2655	2660	2665	2670	2675	2680	2685	2690	2695	2700	2705	2710	2715	2720	2725	2730	2735	2740	2745	2750	2755	2760	2765	2770	2775	2780	2785	2790	2795	2800	2805	2810	2815	2820	2825	2830	2835	2840	2845	2850	2855	2860	2865	2870	2875	2880	2885	2890	2895	2900	2905	2910	2915	2920	2925	2930	2935	2940	2945	2950	2955	2960	2965	2970	2975	2980	2985	2990	2995	3000
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A decorative horizontal border consisting of a repeating pattern of small circles and dots. The pattern is composed of two rows of circles: a top row with larger circles and a bottom row with smaller circles. Interspersed between these rows are small black dots. The pattern is repeated across the width of the border.

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HYDROGRAPH AT STATION A1
PLAN 1. RATIO = 0.50 A1

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
01	15	76	23	24	01	15	76	23	24	01	15	76	23	24
06	25	76	24	25	06	25	76	24	25	06	25	76	24	25
06	35	76	25	26	06	35	76	25	26	06	35	76	25	26
06	45	76	26	27	06	45	76	26	27	06	45	76	26	27
06	55	76	27	28	06	55	76	27	28	06	55	76	27	28
07	05	76	28	29	07	05	76	28	29	07	05	76	28	29
07	15	76	29	30	07	15	76	29	30	07	15	76	29	30
07	25	76	30	31	07	25	76	30	31	07	25	76	30	31
07	35	76	31	32	07	35	76	31	32	07	35	76	31	32
07	45	76	32	33	07	45	76	32	33	07	45	76	32	33
07	55	76	33	34	07	55	76	33	34	07	55	76	33	34
08	05	76	34	35	08	05	76	34	35	08	05	76	34	35
08	15	76	35	36	08	15	76	35	36	08	15	76	35	36
08	25	76	36	37	08	25	76	36	37	08	25	76	36	37
08	35	76	37	38	08	35	76	37	38	08	35	76	37	38
08	45	76	38	39	08	45	76	38	39	08	45	76	38	39
09	05	76	39	40	09	05	76	39	40	09	05	76	39	40
09	15	76	40	41	09	15	76	40	41	09	15	76	40	41
09	25	76	41	42	09	25	76	41	42	09	25	76	41	42
09	35	76	42	43	09	35	76	42	43	09	35	76	42	43
09	45	76	43	44	09	45	76	43	44	09	45	76	43	44
10	05	76	44	45	10	05	76	44	45	10	05	76	44	45
10	15	76	45	46	10	15	76	45	46	10	15	76	45	46
10	25	76	46	47	10	25	76	46	47	10	25	76	46	47
10	35	76	47	48	10	35	76	47	48	10	35	76	47	48
10	45	76	48	49	10	45	76	48	49	10	45	76	48	49
11	05	76	49	50	11	05	76	49	50	11	05	76	49	50
11	15	76	50	51	11	15	76	50	51	11	15	76	50	51
11	25	76	51	52	11	25	76	51	52	11	25	76	51	52
11	35	76	52	53	11	35	76	52	53	11	35	76	52	53
11	45	76	53	54	11	45	76	53	54	11	45	76	53	54
12	05	76	54	55	12	05	76	54	55	12	05	76	54	55
12	15	76	55	56	12	15	76	55	56	12	15	76	55	56
12	25	76	56	57	12	25	76	56	57	12	25	76	56	57
12	35	76	57	58	12	35	76	57	58	12	35	76	57	58
12	45	76	58	59	12	45	76	58	59	12	45	76	58	59
13	05	76	59	60	13	05	76	59	60	13	05	76	59	60
13	15	76	60	61	13	15	76	60	61	13	15	76	60	61
13	25	76	61	62	13	25	76	61	62	13	25	76	61	62
13	35	76	62	63	13	35	76	62	63	13	35	76	62	63
13	45	76	63	64	13	45	76	63	64	13	45	76	63	64
14	05	76	64	65	14	05	76	64	65	14	05	76	64	65
14	15	76	65	66	14	15	76	65	66	14	15	76	65	66
14	25	76	66	67	14	25	76	66	67	14	25	76	66	67
14	35	76	67	68	14	35	76	67	68	14	35	76	67	68
14	45	76	68	69	14	45	76	68	69	14	45	76	68	69
15	05	76	69	70	15	05	76	69	70	15	05	76	69	70
15	15	76	70	71	15	15	76	70	71	15	15	76	70	71
15	25	76	71	72	15	25	76	71	72	15	25	76	71	72
15	35	76	72	73	15	35	76	72	73	15	35	76	72	73
15	45	76	73	74	15	45	76	73	74	15	45	76	73	74
16	05	76	74	75	16	05	76	74	75	16	05	76	74	75
16	15	76	75	76	16	15	76	75	76	16	15	76	75	76
16	25	76	76	77	16	25	76	76	77	16	25	76	76	77
16	35	76	77	78	16	35	76	77	78	16	35	76	77	78
16	45	76	78	79	16	45	76	78	79	16	45	76	78	79
17	05	76	79	80	17	05	76	79	80	17	05	76	79	80
17	15	76	80	81	17	15	76	80	81	17	15	76	80	81
17	25	76	81	82	17	25	76	81	82	17	25	76	81	82
17	35	76	82	83	17	35	76	82	83	17	35	76	82	83
17	45	76	83	84	17	45	76	83	84	17	45	76	83	84
18	05	76	84	85	18	05	76	84	85	18	05	76	84	85
18	15	76	85	86	18	15	76	85	86	18	15	76	85	86
18	25	76	86	87	18	25	76	86	87	18	25	76	86	87
18	35	76	87	88	18	35	76	87	88	18	35	76	87	88
18	45	76	88	89	18	45	76	88	89	18	45	76	88	89
19	05	76	89	90	19	05	76	89	90	19	05	76	89	90
19	15	76	90	91	19	15	76	90	91	19	15	76	90	91
19	25	76	91	92	19	25	76	91	92	19	25	76	91	92
19	35	76	92	93	19	35	76	92	93	19	35	76	92	93
19	45	76	93	94	19	45	76	93	94	19	45	76	93	94
20	05	76	94	95	20	05	76	94	95	20	05	76	94	95
20	15	76	95	96	20	15	76	95	96	20	15	76	95	96
20	25	76	96	97	20	25	76	96	97	20	25	76	96	97
20	35	76	97	98	20	35	76	97	98	20	35	76	97	98
20	45	76	98	99	20	45	76	98	99	20	45	76	98	99
21	05	76	99	100	21	05	76	99	100	21	05	76	99	100
21	15	76	100	101	21	15	76	100	101	21	15	76	100	101
21	25	76	101	102	21	25	76	101	102	21	25	76	101	102
21	35	76	102	103	21	35	76	102	103	21	35	76	102	103
21	45	76	103	104	21	45	76	103	104	21	45	76	103	104

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

MAX FLOW (CFS)	TIME (HR)	MAXIMUM AVE 24-HR
8726.	16.92	6689. 6607. 3317.

14 KK

ROUTE INFLOW HYDROGRAPH THROUGH HOPE LAKE

4.2

HYDROGRAPH ROUTING DATA

15 RS	STORAGE	ROUTING	NUMBER OF SUBREACHES	1	STOR	TYPE OF INITIAL CONDITION	
		ISIPS ATIP ASVRL			64.00	WORKING R AND D COEFFICIENT	
16 SV	STORAGE	0.0	64.0	70.0	100.0	150.0	180.0
17 SE	ELEVATION	417.40	424.70	425.20	426.00	426.70	427.20
18 SO	DISCHARGE	0.	0.	57.	337.	846.	1464.
19 SE	ELEVATION	417.40	424.70	425.20	426.00	426.70	427.20
20 SS	SPILLWAY	CREL SPWID CCON EXPW	424.70 60.00 0.70 1.50	SPILLWAY CREST ELEVATION SPILLWAY WIDTH WEIR COEFFICIENT EXponent OF HEAD			
21 ST	TOP OF DAM	TOPEL OHWTO COPO	426.00 173.00 0.0	ELEVATION AT TOP OF DAM DAM WIDTH WEIR COEFFICIENT			
				EXponent OF HEAD			

					COMPUTED STORAGE-OUTFLOW CURVE		
					100.00	150.00	
	STORAGE	0.0	64.00	70.00	100.00	150.00	180.00
	OUTFLOW	0.0	0.0	57.00	337.00	846.00	1464.00
					210.00	350.00	520.00
					2166.00	4133.00	7442.00
						13216.00	

HYDROGRAPH AT STATION A2

1981, 11(1), 113-126. © 1981 Blackie & Son Ltd.

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW 24-HR	72-HR	2090.
19.50	(CFS)	6-HR 0530.	2160.	2090.

STAGE	TIME	MAXIMUM	AVERAGE	STAGE
STAGE 1 (AC-11)	19.50	6-HR 474.	24-HR 207.	24-HR 202.
STAGE 2 (AC-11)	19.50	6-HR 474.	24-HR 207.	24-HR 202.
STAGE 3 (AC-11)	19.50	6-HR 474.	24-HR 207.	24-HR 202.
STAGE 4 (AC-11)	19.50	6-HR 474.	24-HR 207.	24-HR 202.

CUMULATIVE Akta = 7.70 SC MI

PEAK FLOW AND STAGE (LIND-UF-PERIGO) SUMMARY FOR MULTIPLE PLANE-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND; AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

LOCATION	STATION	AREA	PLAN	RATIOS APPLIED IN FLOWS		
				RATIO 1 0.10	RATIO 2 0.25	RATIO 3 0.50
HYDROGRAPH AT ROUTED TO	A1	7.70	1	Flow	17.82	136.4
	A2	7.70	1	Flow	18.92	16.92
				** PEAK STAGES IN FEET	14.67	14.50
			1	STAGE	27.36	28.87
				TIME	16.32	16.30

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION

A2

PLAN	ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP UF CAM
		424.70 64. 0.	424.70 64. 0.	426.00 100. 337.
RATIO OF FHF TO M.S.ELEV	MAXIMUM RESERVOIR DEPTH OVER DAM	MAXIMUM STORAGE ACFT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS
6.10 0.25 0.50	427.36 426.99 430.93	1.36 2.09 4.93	190. 398. 374.	1699. 8307. 8385.
				TIME OF OUTFLOW HOURS
				9.42 19.47 19.50
				0.0 0.0 0.0

** NORMAL END OF JOB **

APPENDIX 5
REFERENCES

HOPE LAKE DAM

APPENDIX 5
REFERENCES

HOPE LAKE DAM

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